Applied Sciences

# Study of Nano Metal Oxide Incorporated Zinc Phosphate Coatings as Corrosion Inhibitors on Mild Steel

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(Received 30<sup>th</sup> December 2024; Accepted 10<sup>th</sup> February 2025)

### Abstract

The existing corrosion prevention processes and methods are incapable of predicting all environmental conditions. On the other hand, the local metal coating and paint industries continue to suffer from a lack of appropriate advanced phosphating technology as a surface pre-coating technique. The incorporation of ceramic nanoparticles into the phosphate coating has improved the properties such as high corrosion resistance and secondary coating adhesion. As a result, the goal of this research was to create and improve a corrosion prevention method suitable for the metal coating industries by incorporating nano TiO<sub>2</sub> into a phosphate precoating. To facilitate the coating via chemical conversion, the cleaned mild steel specimens were dipped in the prepared phosphating bath containing the nano TiO<sub>2</sub>. Under the given conditions, the optimum coating time was determined to be 90 minutes. Significant changes in coating weight, adhesion quality, surface porosity, and corrosion resistance were observed with the addition of nano TiO<sub>2</sub> (average particle size ~ 25 nm). X-ray Diffraction (XRD), Scanning Electron Microscopy (SEM), and a gemmological microscope were used to investigate the crystal phases and surface morphology of zinc phosphate coatings. XRD data clearly showed that nano TiO<sub>2</sub> has successfully incorporated into the phosphate layer. The addition of nano TiO<sub>2</sub> to the zinc phosphate coating improved its properties, such as coating thickness and surface area, promising an improvement in corrosion resistance. With minor modifications aiming to lower the coating time, the findings of this study could be easily implemented in the metal coating industries and extended to other metals such as steel, aluminium, and alloys.

Keywords: Chemical Conversion, nano -TiO<sub>2</sub>, Mild steel, Phosphating

# 1. Introduction

Corrosion is a natural electrochemical reaction that transforms metal into a stable oxide, damaging its properties [1]. Metals including steel, aluminium, and alloys are commonly affected by corrosion [2]. Corrosion damages the physical and mechanical properties of metals. These include strength, toughness, ductility, appearance etc. Corrosion weakens structures, causes accidents, and leads to failures like pipeline cracks and bridge collapses. Therefore, constant monitoring and prevention of corrosion are crucial. For corrosion prevention, surface treatment processes can be applied to inhibit corrosion [2,19]. This involves treating metal parts before coating them to create a barrier against moisture and air [3]. Surface pretreatment includes mechanical, chemical, or electrochemical treatment before coating processes like electroplating, powder coating or painting [4].

Chemical conversion coatings are preferred surface treatments for metals due to their adherent nature, high coating formation rate, and cost-effectiveness. They can be formed using simple tools and without external electric potential [4]. Types of chemical conversion coatings include Chromate, Phosphate, and Oxalate coatings [5]. Phosphating is commonly used for metal surface treatment. Zinc phosphating, in particular, is widely employed in industries such as automobiles and household appliances. It is favoured for its low cost, easy formation, good corrosion protection, and adhesion [6].

Recent research indicates that nano coatings offer significant potential for enhancing surface corrosion performance compared to micromaterial coatings [7] Nanoparticle-enhanced coatings have demonstrated superior performance, including early-stage corrosion protection, increased resistance, improved control, and controlled inhibitor release [8]. Nano coatings, when applied, result in harder, thicker, tougher surfaces with better adhesive properties, fewer defects, and improved surface corrosion performance compared to micromaterial coatings [7,9].

The next advancement in phosphate coating involves incorporating ceramic nanoparticles to enhance the layer's properties, making it more effective for corrosion prevention and as a pre-coating. This highlights the significant potential for further development and optimization of nanoparticleincorporated zinc phosphating methods. However, for a country like Sri Lanka, relying on imported phosphating solutions—composed of over 90% water—poses an economic challenge for the metal industry. Therefore, this research aims to develop and improve a nanoparticleincorporated formulation for phosphate conversion coating, addressing future needs and local industrial requirements.

## 2. Experimental

# 2.1 Materials

Chemicals including Zinc oxide (ZnO) powder, Nanotitanium dioxide (TiO<sub>2</sub>), 25% Phosphoric acid (H<sub>3</sub>PO<sub>4</sub>), Sodium nitrate (NaNO<sub>3</sub>), Acetone (C<sub>3</sub>H<sub>6</sub>O), Hydrochloric acid (HCl), Sodium hydroxide (NaOH), Sodium chloride (NaCl), Potassium ferricyanide (K<sub>3</sub>[Fe(CN)<sub>6</sub>]), Agar powder, Bromophenol blue, and Phenolphthalein were used in this work and all the chemicals were in analytical reagent grade.

# 2.2 Methodology

The main steps of the phosphating include, metal surface cleaning, phosphating using chemical conversion bath, and characterization of the coating. In this work, we focused primarily on the phosphating step, in which a chemical conversion technique was used to form a phosphate layer on the metal substrates. The phosphate coating process and bath parameters were systematically adjusted to optimize the properties of the coated layers with and without  $TiO_2$ .

#### 2.2.1. Surface cleaning of mild steel

Mild steel specimen was cut into the dimension of 6.0 x 1.0 x 0.4 cm. Then, it was abraded with a series of emery papers up to 400 grits. Then, mild steel sample was degreased and cleaned using a series of chemicals including 10 wt.% *NaOH*, 10% *HCl*, acetone and deionized water respectively, to remove oil, dust, and the remaining rust.

#### 2.2.2. Phosphating bath

The bath composition was originally derived from published research articles [3,8-10,16,20,21,24,25]. Typically, the bath consists of phosphoric acid and zinc oxide as the primary components in an aqueous medium, with sodium nitrate acting as an accelerator. In this study, nano-titanium dioxide was incorporated into the phosphating bath, and a systematic investigation was conducted to determine the optimal bath conditions for achieving an enhanced incorporated nano-TiO<sub>2</sub> zinc phosphate conversion layer.

#### 2.2.3. Phosphating

The dip-coating method was used to coat a layer of zinc phosphate on the steel specimens via chemical conversion. Initially, the dipping time was optimized for the coating in a given bath, without introducing TiO<sub>2</sub> into the bath. The used phosphating bath consists of 0.550 g of zinc oxide mixed with 3.74 ml of phosphoric acid followed by diluting with 100 ml of deionized water. After optimizing the dipping time for a given composition of the bath, different amounts of nano TiO<sub>2</sub> were systematically introduced into the phosphating bath to prepare nano TiO<sub>2</sub> incorporated Zinc phosphate layers. The pH of the phosphating bath was measured and obtained to be 2.98.

#### 2.2.4. Characterization of phosphate coating

The effects of introducing nano TiO<sub>2</sub> into the optimized phosphating bath on composition, coating weight, surface morphology and corrosion resistance were assessed through various methods. A destructive method was employed to evaluate coating weight with respect to immersion time. Two sets of phosphate-coated samples were used to compare the corrosion resistance of specimens with and without TiO<sub>2</sub> incorporation. The specimens were immersed in a Ferroxyl reagent test to evaluate surface porosity and monitor corrosion progression on both coated and uncoated areas. Additionally, X-ray diffraction (XRD) analysis was performed to determine the crystal phases present in the phosphate coating. The XRD analysis covered a diffraction angle range of  $2\theta$  from  $0^{\circ}$  to  $100^{\circ}$  using Cu K $\alpha$  radiation ( $\lambda$ = 1.5406 Å) and was conducted using the Ultima IV X-Ray Diffractometer. The surface morphology of the zinc phosphate coatings was examined using scanning electron microscopy (SEM) and a gemmological microscope.

#### 3. Results and Discussion

#### 3.1. Optimum bath composition

Chemical composition and relevant control parameter that were used to obtain an optimum nano-TiO<sub>2</sub> incorporated zinc phosphate conversion layer is tabulated in the Table-1. Here, the calculations are shown for a total bath volume of 100 ml.

#### Table 1

Chemical composition and control parameters

Chemical Composition					
25.0 % <i>H</i> <sub>3</sub> <i>PO</i> <sub>4</sub>	3.74 ml				
ZnO	0.550 <i>g</i>				
NaNO <sub>3</sub>	0.147g				
Nano $TiO_2$ (25 nm)	0.200g				
Deionized water	100.0ml				
Control Parameters					
рН	$2.98\pm0.1$				
Temperature	27.0°C ± 3.0°C				
Immersion time	1. 30 hours				
Free acid value (FA)	$1.4 \ cm^3$				
Total acid value(TA)	16. 2 $cm^3$				
FA: TA	1:11.6				



**Fig. 1**. (a) Depicts the effect of growth time on coating weigh, coating area is  $11.6 \text{ cm}^2$ , (dashed line represent a liner fit to the graph of weight vs time), (b) Comparison of the phosphate coating weight without (coating area  $11.6 \text{ cm}^2$ ) and with TiO<sub>2</sub> (coating area  $9.8 \text{ cm}^2$ ), (inset image of the Fig. 1 (b) shows the microscopic images of the prepared phosphate specimens)

#### 3.2. Coating weight vs time

Fig. 1 exhibits the phosphate coating over time for timeseries samples without TiO<sub>2</sub> incorporation. Under these conditions, the optimal coating time was observed as 90 minutes. After about 90 minutes under these conditions, the growth or the coating thickness reaches its maximum. This may be attributed to the obstruction of the active metal surface by the deposited layer. Alternatively, it could result from the equilibrium between growth and dissolution reactions, influenced by the substantial presence of free acid in the solution. The phosphate coating amount was assessed by comparing the apparent weight before and after coating of a given area. The calculated average coating weight of the samples (without TiO<sub>2</sub>) is about 11 mg (coating area 11.6  $cm^2$ ). The samples prepared with the addition of nano-TiO<sub>2</sub> into the bath and after 90 minutes of coating, showed a coating weight of about 37 mg (coating area 9.8 cm<sup>2</sup>). It represents approximately a fourfold increase in coating weight and thickness compared to standard zinc phosphate coatings per unit area. The presence of white material in the microscopic image (inset Fig. 1 (b)) indicates the incorporation of TiO<sub>2</sub> particles into the phosphating layer. For optimal adhesion and corrosion resistance, zinc phosphate coatings serve as an effective pre-coating before secondary applications like powder coating, with a desired thickness of 5 to 15 µm. This study highlights that using a bath containing nano-TiO<sub>2</sub> can achieve the minimum target thickness in approximately 12 minutes of growth.

# 3.3. Surface morphology of normal and nano TiO<sub>2</sub>- zinc phosphate coating - SEM

Fig. 2(a) and (b) exhibit SEM images of phosphate coating on mild steel without  $TiO_2$  at magnifications of 500x and 4500x, respectively. Fig. 2(c) and (d) show the SEM images of specimens with  $TiO_2$ , at magnifications of 500x and 1000x, respectively. These SEM images provide valuable insights into the nucleation and growth process of phosphate coatings on the mild steel substrate. The visible

crystals in Fig. 2(a) and 2(c) are identified as phosphate compounds within the coatings. Without nano- $TiO_2$  in the bath large crystals exceeding 10 µm in size, with an average dimension of approximately 20  $\mu$ m  $\times$  30  $\mu$ m, and distinct 3D particle edges are clearly observed on the surface. This suggests that long-range, three-dimensional growth is more favourable when foreign materials or impurities such as nano-TiO<sub>2</sub> are absent in the bath. However, the crystals formed in this condition are randomly oriented on the metal surface. Conversely, with the introduction of nano-TiO<sub>2</sub> into the phosphating bath, only a few rod-like crystals exceeding 10 µm in length are clearly visible on the surface, while most other crystal formations appear smaller than 10 µm in size. The distinct modification in the formed crystals in the presence of TiO<sub>2</sub> suggests significant changes in the nucleation and growth mechanisms. In the presence of nano-TiO<sub>2</sub>, the nucleation density has increased significantly, while the crystal size is restricted to a few micrometres, effectively limiting three-dimensional growth. The resulting coating exhibits, higher thickness with a more homogeneous surface and well-defined, small rod-like crystals.

Similar studies reveal that incorporating various additives, such as cations (Ni<sup>2+</sup>, Mn<sup>2+</sup>) [11], TiO<sub>2</sub> [10,30], CeO [12], and nano-SiO<sub>2</sub> [13,17,27], significantly modify the properties of phosphate conversion coating layers. These modifications result in improved layer uniformity, increased thickness and growth rate, fewer defects, and refined crystal structures with minimal porosity. The addition of nanoparticles or suitable additives is believed to influence the growth mechanism by increasing nucleation density and reducing large 3D crystal growth. The physical adsorption of nanoparticles (e.g., TiO<sub>2</sub>, ZnO) onto the metallic surface forms cathodic regions, enhancing hydrogen evolution and promoting the precipitation of phosphate crystals. A higher concentration of adsorbed nanoparticles increases the number of phosphate crystal nuclei, enhancing nucleation



Fig. 2. (a) and (b) exhibits the SEM images of phosphate coating on mild steel without  $TiO_2$ , (magnification 500x and 4500x, respectively). (c) and (d) exhibits the SEM images of phosphate coating on mild steel with  $TiO_2$ , (magnification 500x and 1000x, respectively). Thicknesses of the coating layers are shown with horizontal bars drawn in cross sectional SEM images of (b) and (d).

density and resulting in smaller crystal sizes in the phosphate coating [13,22,23]. Consequently, large 3D crystal growth is suppressed, while the formation of smaller crystallites is enhanced, as evidenced by SEM images in this and other studies.

The SEM image of the sample cross-section in Fig. 2(d) confirms a dense and uniform coating with a thickness of approximately 45  $\mu$ m in the presence of TiO<sub>2</sub>, whereas samples without TiO<sub>2</sub> exhibit an average thickness of about 11  $\mu$ m. Adding nano-TiO<sub>2</sub> to the phosphating bath enhances the degree of crystalline coverage by reducing the grain size

and minimizing the voids of the phosphate coating. Fine surface structures may increase the effective surface area of the metal substrate, which is crucial for improved adhesion of subsequent paint or coating layers and various applications. Notably, the addition of nano-TiO<sub>2</sub> particles has increased the coating thickness by approximately four times compared to samples without TiO<sub>2</sub>, aligning with the coating weight data. This is advantageous in commercial applications as it allows to produce high-quality thick layers in a shorter time, resulting in cost reduction and higher profitability.

Table 2	
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Comparison of XRD peak positions of various phases in phosphate coatings with reference data

Crystalline Phases	H (Hopeite)	P (Phosphophyllite)	Zn (Zinc)	ZPH (Zinc phosphate Hydrate)	T (TiO <sub>2</sub> )
Without TiO <sub>2</sub>	24.75, 30.50, 43.75, 59.85, 81.50,	33.05, 49.10	38.60	8.75, 15.80, 18.50	-
WithTiO <sub>2</sub>	31.05, 46.60, 60.30, 81.95	34.05	39.10	9.40, 19.10, 64.75, 81.95	9.40, 19.10, 26.00, 34.05, 44.40, 64.75, 81.95
Reference data [8,11]	22.60, 24.80, 30.50, 44.20, 46.20, 59.80, 65.20	20.2, 34.4, 45.5, 60.9		9.40, 16.40, 18.60, 19.60, 46.20	25.90, 47.10, 37.10, 62.20, 69.70

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Fig. 3. XRD patterns of the phosphate coating on mild steel substrate, (a) without TiO<sub>2</sub>, and (b) with TiO<sub>2</sub>.

#### 3.4. Crystal phases in the phosphate coatings - XRD

Fig. 3 (a) and (b) shows the XRD profile of the top surface of the zinc phosphate coating with and without incorporation of nano- TiO<sub>2</sub>. It is shown that the phosphate coating mainly consists of Hopeite  $[Zn_3(PO_4)_2, 4H_2O]$ , phosphophyllite [Zn<sub>2</sub> Fe (PO<sub>4</sub>)<sub>2</sub>. 4H<sub>2</sub>O], and zinc phosphate hydrate [Zn<sub>3</sub>(PO<sub>4</sub>)<sub>2</sub>. H<sub>2</sub>O] [3,8,14]. Fig. 3(b) clearly depicts additional phases (represented by 'T') that are likely associated with the incorporation of TiO<sub>2</sub> into the layer. Peaks related to TiO<sub>2</sub> representing mixed phases of both rutile and anatase. Table 2 shows the XRD crystal phases position compared with some literature data available for zinc phosphate coatings with and without incorporation of nano- TiO<sub>2</sub> [8,11]. The observed phases of the phosphate coating align well with the available literature data. Moreover, the presence of nano- TiO2 particles has led to an increase in the intensity of these phases.

# 3.5. Surface porosity of the coatings - Ferroxyl reagent test

Fig. 4 displays the results of the Ferroxyl test, which is employed to identify surface porosity in coatings. This method was based on formation of blue spots on an agar medium dipped in potassium ferricyanide, hydrochloric acid, distilled water and phenolphthalein mixture when applied over the phosphate coated specimen for one day.  $Fe^{2+}$  reacts with ferricyanide ions (Fe(CN)<sub>6</sub><sup>3-</sup>) to form Prussian Blue (Fe<sub>4</sub>[Fe(CN)<sub>6</sub>]<sub>3</sub>) and blue spots indicate the presence of Fe<sup>2+</sup>. The porosity is quantified by the number of blue spots per square centimetres [15]. In this study, the analysed top-side area of the phosphate-coated samples with and without  $TiO_2$  was measured as 3.4 cm<sup>2</sup> and 4.0 cm<sup>2</sup>, respectively. The uncoated areas of the two specimens are 2.2 cm<sup>2</sup> and 1.8 cm<sup>2</sup> for the samples with and without  $TiO_2$ , respectively. No color change was observed around the coated area even after one day, indicating the absence of



Fig. 4. Progression of the corrosion with the Ferroxyl regent test. (a) Before the test, (b) after five minutes, and (c) after 24 hours of starting the test.

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significant porosity in both types of zinc phosphate layers, with and without  $TiO_2$ . However, color changes were noticed around the uncoated area due to the presence of  $Fe^{+2}$  ions generated through oxidation. The findings of this study suggest that, under preliminary testing conditions, both coatings with and without nano- $TiO_2$  exhibit minimal porosity and are adequately suitable as pre-coating layers. However, coating weight analysis and SEM analysis indicates that the nano- $TiO_2$  incorporated layers have greater thickness, improved crystallite structure, and possibly a higher effective surface area, along with an enhanced growth rate. This increased growth rate is particularly beneficial for industrial applications, offering improved efficiency and cost-effectiveness in large-scale coating processes.

# 4. Conclusion

Zinc phosphate coating is a widely utilized surface pretreatment method in metals prior to top coating. The next generation of phosphating involves the integration of ceramic nanoparticles into the phosphate layers. This study demonstrates that the incorporation of nano- TiO2 significantly enhances the effective surface area, layer thickness, and homogeneity, crucial factors for secondary coatings. When nano- TiO<sub>2</sub> is added to the phosphating bath, it reduces the size of the nano zinc phosphate crystals, activating the surface of mild steel. Corrosion studies indicate that the prepared layers exhibit minimal porosity, ensuring high-quality coatings. Additionally, the presence of nano- TiO<sub>2</sub> promotes faster growth, making it favourable for industrial applications. In the future, we aim to further reduce the growth time by increasing bath concentrations while maintaining the free acid value at an optimal level to minimize reverse reactions. Additionally, we plan to conduct standard characterizations, such as salt spray testing and crosscut adhesion tests, in collaboration with metal coating industries to ensure the commercial viability of these findings.

### **Conflict of Interest**

No conflicts of interest to declare.

#### Acknowledgements

The authors express their gratitude to the Faculty of Applied Sciences at Uva Wellassa University of Sri Lanka for providing laboratory facilities. They also extend their appreciation to Mr. Dinusha Liyanarachchi, Director of Business Development at Trendy Solutions (Pvt) Ltd., Sri Lanka, for his valuable insights and discussions. Special thanks are given to Prof. P.M. Sirimanne, Department of Science and Technology at Uva Wellassa University, for supplying some chemicals.

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